Listing of Claims:

- (Previously Presented) An exterior surface treated article comprising a bulksolidifying amorphous alloy having a mechanically treated exterior surface and having improved durability and fatigue resistance over a similar article without said mechanically treated exterior surface, the mechanically treated exterior surface comprising a plurality of deformations in the exterior surface.
- (Previously Presented) The article of claim 1, wherein the deformations result from a mechanical surface treatment process applied to the exterior surface.
- (Previously Presented) The article of claim 2, wherein the surface treatment process is a shot-peening process.
- (Previously Presented) The article of claim 3 wherein the shot-peening process comprises a shot having a diameter of approximately 0.006 inches to 0.040 inches.
- (Previously Presented) The article of claim 1 wherein the treated article is a golf club face insert or a shaft.
- 6. (Original) The article of claim 1 wherein the surface treatment process is a laser shock peening process, wherein the deformations are formed by a shock wave that ablates a portion of the exterior surface.
- 7. (Original) An article of bulk-solidifying amorphous alloy having an exterior surface with a plurality of deformations therein, wherein the deformations alter the exterior surface such that the article has improved durability and fatigue resistance as compared to a substantially identical article lacking the deformations in the exterior surface.
- (Previously Presented) A method of improving the durability and fatigue resistance of an exterior surface treated article made from bulk-solidifying amorphous alloy, comprising:

applying a shot-peening process to at least a portion of an exterior surface of the article; and

creating a plurality of deformations in the exterior surface by mechanically compressing a plurality of shots against the exterior surface to create a mechanically treated exterior surface,

wherein the article has an improved durability and fatigue resistance over a similar article without said mechanically treated exterior surface.

- (Previously Presented) The article of claim 3, wherein the shot-peening process is applied to a substantial portion of the exterior surface.
- 10. (Previously Presented) The article of claim 1, wherein the improved durability and fatigue resistance is demonstrated as improved peak load for failure and increased cycles to failure under fatigue cycling.
- (Previously Presented) The article of claim 10, wherein a ratio of the peak load for failure of the article versus the similar article is over 33/23.
- 12. (Previously Presented) The article of claim 10, wherein a ratio of the peak load for failure of the article versus the similar article is over 33/27.
- 13. (Previously Presented) The article of claim 10, wherein a ratio of the cycles to failure under fatigue cycling of the article versus the similar article is more than 30/2.
- 14. (Previously Presented) The article of claim 10, wherein a ratio of the cycles to failure under fatigue cycling of the article versus the similar article is more than 30/9.
- 15. (Previously Presented) The article of claim 10, wherein a ratio of the cycles to failure under fatigue cycling of the article versus the similar article is more than 15/2.
- 16. (Previously Presented) The article of claim 10, wherein a ratio of the cycles to failure under fatigue cycling of the article versus the similar article is more than 15/5.

- 17. (Previously Presented) The article of claim 10, wherein a ratio of the cycles to failure under fatigue cycling of the article versus the similar article is more than 30/5.
- 18. (Previously Presented) The article of claim 1, wherein the bulk-solidifying amorphous alloy comprises a ferrous alloy.
- (Previously Presented) The article of claim 1, wherein the bulk-solidifying amorphous alloy comprises a Ni-containing alloy.
- (Previously Presented) The article of claim 18, wherein the bulk-solidifying amorphous alloy is a ferrous alloy comprising Fe, Ni and Co.
- 21. (Previously Presented) The article of claim 1, wherein the bulk-solidifying amorphous alloy has the glass transition temperature of 550°C or above.
- (Previously Presented) The article of claim 1, wherein the bulk-solidifying amorphous alloy has the glass transition temperature of 500°C or above.
- 23. (Previously Presented) The article of claim 22, wherein the bulk-solidifying amorphous alloy comprises a composition being represented by the following general formula: Ni_a (Zr_{1x} $Ti_x)_b$ Si_c

where a, b and c are atomic percentages of nickel, zirconium plus titanium and silicon, respectively, and x is an atomic fraction of titanium to zirconium, wherein;

45 atomic $\% \le a \le 63$ atomic %,

32 atomic $\% \le b \le 48$ atomic %,

1 atomic % < c < 11 atomic %, and

 $0.4 \le x \le 0.6$.

- (Previously Presented) The article of claim 23, wherein the bulk-solidifying amorphous alloy further comprises V, Cr, Mn, Cu, Co, W, Sn, Mo, Y, C, B, P, Al, or combinations thereof.
- 25. (Previously Presented) The article of claim 22, wherein the bulk-solidifying amorphous alloy comprises a composition being represented by the following general formula:

where d, e and f are atomic percentages of nickel, zirconium plus titanium and phosphorus, respectively, and y is an atomic fraction of titanium to zirconium, wherein;

- 50 atomic $\% \le d \le 62$ atomic %,
- 33 atomic $\% \le e \le 46$ atomic %,
- 3 atomic $\% \le f \le 8$ atomic %, and
- $0.4 \le y \le 0.6$.